



# Aerodynamic parameters and sensible heat flux estimates for a semi-arid ecosystem

John H. Prueger<sup>a,\*</sup>, William P. Kustas<sup>b</sup>, Lawrence E. Hipps<sup>c</sup>,  
Jerry L. Hatfield<sup>a</sup>

<sup>a</sup> USDA-ARS National Soil Tilth Laboratory, 2150 Pammel Drive, Ames, IA, USA

<sup>b</sup> USDA-ARS Hydrology and Remote Sensing Laboratory, Beltsville, MD, USA

<sup>c</sup> Plant, Soils and Biometeorology, Utah State University, Logan, UT, USA

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## Abstract

Aerodynamic parameters of roughness length ( $z_0$ ) and displacement height ( $d_0$ ) for semi-arid grassland, mixed grass–mesquite and mesquite rangeland were computed from eddy covariance measurements of sensible heat flux ( $H$ ), standard deviations of vertical velocity and air temperature ( $\sigma_w$  and  $\sigma_T$ ), and mean wind speed ( $u$ ) within the framework of Monin–Obukhov similarity theory. Reasonable estimates of  $z_0$  were obtained for all sites but unrealistic  $d_0$  values resulted for most sites except mesquite. Independent estimates of  $z_0$  and  $d_0$  were also determined at the mesquite site with a traditional wind speed profile method and compared with results computed from an approach using laser altimeter data. Results showed good agreement among approaches. Also, within the framework of flux–variance using,  $\sigma_T$ , and derived  $z_0$ ,  $d_0$  with  $u$ , computed  $H$  fluxes were evaluated and compared to eddy covariance measurements.

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**Keywords:** Aerodynamic roughness length; Displacement height; Friction velocity; Eddy covariance; Mesquite dune

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## 1. Introduction

The energy and water balances of native surfaces are strongly coupled to hydrology and climate as well as other biological and physical processes related to

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\*Corresponding author. Tel.: +1-515-294-7694; fax: +1-515-294-8125.

E-mail address: prueger@nsl.gov (J.H. Prueger).

ecosystem structure and function. Heat, water and momentum exchange at a surface are turbulent processes often estimated from vertical gradients of temperature, water vapor and wind speed above the surface using flux–gradient relationships. These processes are non-linear and are related to soil moisture conditions, canopy structure, vegetated land cover distribution, topography (micro- and meso-scale) and surface albedos (Campbell and Norman, 1998).

With a flux–gradient approach, surface roughness and heterogeneity are typically characterized by two aerodynamic parameters, aerodynamic roughness length,  $z_0$ , and zero-plane displacement height ( $d_0$ ). Aerodynamic roughness length relates to the efficiency of momentum exchange at the surface and  $d_0$  represents the effective height of momentum absorption within the roughness elements (Campbell and Norman, 1998). Both  $z_0$  and  $d_0$  are important in aerodynamic formulations for modeling energy exchange processes across the soil–vegetation–atmosphere continuum. This is especially the case for models developed to estimate turbulent exchange processes for sparsely vegetated heterogeneous surfaces in semi-arid landscapes (Shuttleworth and Wallace, 1985).

Vegetation height, structure, density and landscape topography affect roughness parameters (Brutsaert, 1982). Estimating  $z_0$  and  $d_0$  is difficult but especially so for landscapes comprised of sparse or patchy vegetation typical of arid and semi-arid regions. Compared to agricultural crops, few studies have evaluated  $z_0$  and  $d_0$  for native desert grass and shrub communities (Wieringa, 1993). Some studies have evaluated aerodynamic parameters using wind profile approaches and flux–variance relations for desert environments (Weaver, 1990; Kustas et al., 1994).

The traditional logarithmic wind profile approach uses multiple levels of wind speed measurements to mathematically solve for  $z_0$  and  $d_0$  by minimizing the sum of square errors for wind speed and measurement height (Robinson, 1962; Stearns, 1970). Haenel (1993) proposed an iterative approach following Robinson (1962) to account for non-neutral conditions, and thus can use all data for the range of stabilities found during the course of a diurnal cycle. However, the approach is not likely to be applicable to heterogeneous surfaces where profiles of mean wind speed and scalars do not appear to follow Monin–Obukhov similarity thus violating important underlying assumptions of the wind profile method (e.g., Chen and Schwerdtfeger, 1989; Tsvang et al., 1998). Possible reasons can include; (1) surface heterogeneity effects producing a weakly developed equilibrated boundary-layer above a surface; (2) tower height limitations and the depth of a fully adjusted boundary-layer (FAL) over a surface can be such that measurements believed to be made in the FAL are in actuality made in the roughness sub-layer and thus subject to significant errors; (3) non-uniformity of vertical sources and sinks of heat and water vapor within sparse canopies are poorly defined as a single layer. For example, Kustas et al. (1998); Hipps and Kustas (2001) reported significant departures of observed temperature profiles for a coppice dune site under unstable conditions from those defined by Monin–Obukhov similarity theory. This may have resulted from large spatial variations of surface temperatures between dune and inter-dune spaces producing considerable scatter in the universal stability functions (e.g., Tsvang et al., 1998). In semi-arid landscapes, potential logistical and theoretical limitations

inherent to wind profile techniques necessitates alternative approaches for estimating aerodynamic roughness parameters.

One such approach described by Weaver (1990) makes use of flux–variance relationships using eddy covariance measurements of scalar fluxes and turbulence statistics. However, Weaver (1990) only describes estimating one of the two aerodynamic roughness parameters, namely  $z_0$  and does not explicitly evaluate the role of  $d_0$  in the flux–variance equations. For most landscapes, the impact of the roughness elements (vegetation and topography) on momentum transport should include the effect of both aerodynamic roughness parameters in Monin–Obukhov similarity relations (Brutsaert, 1982).

In this paper, we evaluate a flux–variance approach using eddy covariance measurements of  $H$ , mean wind speed ( $u$ ), the standard deviation of vertical wind speed and air temperature ( $\sigma_w$ ,  $\sigma_T$ ), to estimate aerodynamic roughness parameters ( $z_0$ , and  $d_0$ ) and  $H$  using turbulent statistics for a semi-arid grassland, a transitional site containing a mixture of grasses and shrubs and a honey mesquite coppice dune site in a Northern Chihuahuan desert.

## 2. Theory

Using Monin–Obukhov similarity theory in the surface layer (10's of meters above a surface) the wind profile (i.e. traditional wind profile approach) is commonly assumed to be logarithmic (Brutsaert, 1982) and is expressed as

$$\bar{u} = \frac{u_*}{k} \ln \left[ \frac{z - d_0}{z_0} \right] - \psi_m(\zeta), \quad (1)$$

where  $\bar{u}$  is mean wind speed ( $\text{m s}^{-1}$ ),  $u_*(\tau/\rho)^{1/2}$  ( $\text{m s}^{-1}$ ) friction velocity,  $\tau$  surface shear stress ( $\text{kg m}^{-1} \text{s}^{-2}$ ),  $\rho$  density of air ( $\text{kg m}^{-3}$ ),  $k$  von Karman's constant (0.4, dimensionless),  $z$  measurement height above a surface (m),  $z_0$  roughness length (m) and  $d_0$  the zero-displacement height (m),  $\Psi_m(\zeta)$  is a stability function that accounts for buoyancy effects on the wind profile (for a review, see Höglström, 1988, 1996) where  $\zeta = z - d_0 / L$  and  $L$  is the Monin–Obukhov length (m) (Monin and Obukhov, 1954), that defines the surface boundary layer stability in terms of turbulent fluxes of heat and water as

$$L = - \frac{u_*^3 \rho}{kg[(H/T_A C_p) + +0.61E]}, \quad (2)$$

where  $g$  is acceleration due to gravity, ( $\text{m s}^{-2}$ ),  $H$ , sensible heat flux ( $\text{W m}^{-2}$ ),  $T_A$ , air temperature (K),  $C_p$  specific heat of air ( $\text{J kg}^{-1} \text{K}^{-1}$ ),  $E$  is the rate of surface evaporation ( $\text{kg m}^{-2} \text{s}^{-1}$ ) and all other terms have been previously defined.

Flux–variance relations were derived from Monin–Obukhov similarity theory to estimate momentum and sensible heat fluxes (Tillman, 1972) and have been used for water vapor and other scalar fluxes (Wesley, 1988). Further refinements to the technique have been developed (e.g., De Bruin et al., 1993). Early investigations indicated the approach does not work as reliably for latent heat flux (evaporation)

relative to sensible heat flux when applied over heterogeneous surfaces, particularly sparse canopy-covered landscapes typical of arid and semi-arid landscapes (Weaver, 1990). In addition, some studies indicate that the “universal” constants for the flux–variance formulations of sensible heat flux varies with surface type and condition (De Bruin et al., 1991; Weaver, 1990; Padro, 1993).

Under moderately unstable conditions ( $z-d_0/L < 0$ ), the equation relating  $H$  to temperature variance ( $\sigma_T$ ) has the following form (Tillman, 1972):

$$H = \rho C_P u_* \left( \frac{\sigma_T}{C_1} \right) \left[ C_2 - \frac{z-d_0}{L} \right]^{1/3}, \quad (3)$$

where  $C_1$ ,  $C_2$  are “universal” dimensionless constants derived experimentally and all other terms have been previously defined. For strongly unstable condition typically found in arid and semi-arid environment (i.e., free convective case where  $z-d_0/L \ll 0$  and  $u_* \rightarrow 0$ ) Eq. (3) is expressed:

$$H = \rho C_P \left[ \left( \frac{\sigma_T}{C_1} \right)^3 \frac{kg(z-d_0)}{T_A} \right]^{1/2}, \quad (4)$$

where all terms have been previously defined. Using Monin–Obukhov similarity theory, a relationship is also derived for unstable conditions relating the variance of vertical wind velocity ( $\sigma_w$ ) to the friction velocity  $u_*$  (Panofsky and Dutton, 1984):

$$u_* = \frac{\sigma_w}{C_3(1 - C_4(z-d_0)/L)^{1/3}}. \quad (5)$$

As in previous similar expressions, the universal constants  $C_3$  and  $C_4$  are dimensionless and are derived experimentally.

The magnitude of  $C_1$  is found in the literature to range from approximately 0.9 (Padro, 1993) to 1.25 (Wesley, 1988) with a generally accepted literature value of 0.95 (Wyngaard et al., 1971). For heterogeneous surfaces, the values of  $C_2$ ,  $C_3$  and  $C_4$  have been reported to be  $\sim 0.04$ , 1.25, and 3 respectively (De Bruin et al., 1993).

Using the above set of equations and eddy covariance measurements of  $H$  and  $\sigma_w$ , previous studies have reported aerodynamic roughness parameters of  $z_0$  and  $d_0$  for similar semi-arid rangeland environments (Weaver, 1990; Kustas et al., 1994). However, mesquite dune landscapes have not been addressed. The procedure for estimating  $z_0$  and  $d_0$  is summarized as follows; initial values of  $z_0$  and  $d_0$  are selected from the literature (De Bruin et al., 1993), an iterative loop is conducted where  $L$  is computed from Eq. (2) using EC measurements of  $H$ , and  $\lambda E$  ( $H_M$ , and  $\lambda E_M$ , where  $\lambda$  is the latent heat of vaporization  $\sim 2.45 \times 10^6 \text{ J kg}^{-1}$  and subscript  $M$  signifies measured) and  $u_*$  is computed from the EC measurement of  $\sigma_w$  and Eq. (5) ( $u_{*V}$ ); a solution is defined when there is negligible change in the magnitude of  $L$  and  $u_*$ . Computed sensible heat flux  $H$  can now be estimated from Eq. (3) ( $H_V$ ), and  $u_*$  from Eq. (1) ( $u_{*U}$ ), which contains the initial estimate of  $z_0$ . The appropriate values of  $z_0$  and  $d_0$  are found when the ratios of  $H_V/H_M$  and  $u_{*V}/u_{*U}$  approach unity.

### 3. Materials and methods

#### 3.1. Site description

The Jornada Experimental Range (JER) is approximately 35 km northeast of Las Cruces, New Mexico on the Jornada del Muerto Plain of the Chihuahuan Desert. This is the largest desert (453,250 km<sup>2</sup>/175,000 mi<sup>2</sup>) in North America and is mostly located in Mexico and stretches into parts of the southwest United States. The JER was established in 1912 by the United States Department of Agriculture (USDA) and is part of the Agricultural Research Service (ARS) and the long-term Ecological Research (LTER) Program administered by the National Science Foundation (NSF).

The Jornada LTER site is primarily a semi-arid grassland (black grama) encompassing approximately 78,000 ha. The climate is characteristic of the northern region of the Chihuahuan desert and is the most arid of the North American grasslands. These grasslands are fragile dynamic systems and are sensitive to natural and anthropogenic influences. An example can be observed in the northern extent of the Chihuahuan desert where grass communities dominated by black grama (*Bouteloua eriopoda* (Torr.) Torr.) have experienced a gradual encroachment by honey mesquite (*Prosopis glandulosa* Torr.) shrubs in a process initiated by drought and aggravated by overgrazing practices during the last century (Buffington and Herbel, 1965; Gibbens et al., 1992). Increased landscape roughness from dune formation as well as a change in vegetation type (grasses to shrubs) likely alter the wind flow characteristics near the surface and may increase surface roughness and affect turbulent exchange with the lower boundary-layer of the atmosphere. Three sites were selected for intensive studies as part of the JORNEX project (Ritchie et al., 1998; Rango et al., 1998). The sites represented grass, shrub (honey mesquite), and a grass–shrub transition zone. Black grama was the dominant species for the grass site (referred to as grass-1) and was located within an enclosure to prevent animal grazing. Honey mesquite on coppice dunes represented the shrub site (referred to as mesquite site). The dunes vary in height from 0.75 to 2.5 m with honey mesquite growing on the tops of each dune. The transition site was comprised of a mix of vegetation components from both grass and mesquite sites with dunes in the initial stages of development not exceeding 0.5 m in height. During one of the field campaigns (September, 1996) two additional sites, one containing grass which was grazed (referred to as grass-2) and another with a variety of shrub species but no dune formation (referred to as shrub site) were also instrumented for surface energy flux measurements.

#### 3.2. Vegetation measurements

Measurements of vegetation composition (species), cover, and height (*h*) were made along 150-m transects established at each JORNEX site using vertical line intercept techniques (Canfield, 1941; Eberhart, 1978). Permanent markers were geopositioned so that the same transects were measured during each campaign.

Along each transect three 30-m segments were measured for vertical line intercepts at 10-cm intervals for a total of 900 points per transect. Height measurements (nearest cm) of live plant material and standing litter were recorded by species. Since vegetated coppice dunes had substantially more relative relief, cross-sectional 100-m engineering survey results were combined with laser altimeter data to obtain an mean estimate of dune topography and mesquite vegetation height. Leaf area index (*LAI*) measurements were made along each transect with a non-destructive optical *LAI* sensor. *LAI* values were 1, 0.4 and 0.5 for the grass-1, mesquite and transition sites respectively. *LAI* measurements were not available for the grass-2 and shrub sites. For more detailed information on vegetation measurements see [Havstad et al. \(2000\)](#).

The vegetation measurements made at the three main sites (i.e., grass-1, mesquite and transition site) including the engineering transect for the mesquite site provided an estimate of mean vegetation/obstacle heights. For the mesquite site, dune heights ranged from 0.3 to 2 m with an average dune height of 0.85 m. The mesquite is clumped on the tops of the dunes, and when the vegetation height is added to the dune height, the range was from 1.1 to 3.5 m with an average total dune plus mesquite height of 1.8 m. The grass-1 site had a mean canopy height of 0.1 m while the mean canopy height at the transition site was 0.4 m. The grass-2 and shrub site average canopy heights were estimated to be approximately 0.1 and 0.5 m respectively.

### 3.3. Surface energy balance measurements

During intensive field campaigns sensible and latent heat fluxes ( $H$  and  $LE$ ) were measured using eddy covariance (EC) at all sites. Measurements were made with one-dimensional (1-D) sonic anemometers (with a fine wire thermocouple) and krypton hygrometers. In addition the EC instruments provided measurements of the variances of vertical wind speed,  $\sigma_w$ , and air temperature,  $\sigma_T$  ([Tanner et al., 1985](#); [Tanner, 1988](#)). The EC instruments were deployed 2 m above the local terrain at all sites except the mesquite site where sensors were mounted 3 m above the highest mesquite vegetation on a 10 m tower. Measurements of net radiation,  $R_n$ , air temperature, relative humidity, wind speed and direction were made the same heights as the EC measurements. Soil heat flux,  $G$ , was measured at each site using heat flux plates placed 0.08 m below the soil surface. Heat storage in the soil layer above the heat flux plates was computed using soil temperatures measured with thermocouples at depths of 0.02 and 0.06 m below the surface (and above the soil heat flux plate) and gravimetric estimates of soil water content and thermal conductivity ([Hanks and Ashcroft, 1980](#)). In addition, the 10-m tower erected at the mesquite dune site was also instrumented with cup anemometers and aspirated air temperature sensors at 3, 4, 5, 6, 8, and 10 m above the mesquite vegetation. Wind speed and temperature profile data were used to compute stability corrections ( $\Psi_m(\zeta)$ ) to the profile data ([Högström, 1988, 1996](#)) and aerodynamic roughness parameters using the traditional wind profile iterative least square errors technique ([Robinson, 1962](#); [Kustas et al., 1989](#); [Hatfield, 1989](#)). For additional profile measurement details, see [De Vries et al. \(2001\)](#).

The EC measurements were scanned at 10 Hz with intermediate calculations of the variances and covariances computed every 10 min and averaged as 30-min output of  $H$ ,  $\lambda E$ ,  $\sigma_w$  and  $\sigma_T$ . All other measurements were scanned at 10 s and output as 30-min averages. Preliminary analysis of the EC data from the grass-1 and mesquite sites are described by Prueger et al. (1998).

## 4. Results

### 4.1. Estimating $d_0$ and $z_0$

Initial values of the dimensionless constants  $C_1$ ,  $C_2$ ,  $C_3$ ,  $C_4$  selected for the flux–variance procedure are provided in Table 1 from De Bruin et al. (1993). In this study we confined our analysis to the unstable-free convective condition range, only data with measured sensible heat flux ( $H_M$ )  $> 50 \text{ W m}^{-2}$  were selected and used for estimating the roughness parameters. Canopy/obstacle heights,  $h$ , from the vegetation measurements and engineering surveys, and estimates of  $d_0$  and  $z_0$  using the procedure described above are presented in Table 2. The magnitudes of  $z_0$  were similar to literature values reported for native grass and shrub land ecosystems in semi-arid regions (Weaver, 1990). However, the magnitude of  $d_0$  for three of the five sites was larger than the estimated mean vegetation height (Table 2). This is not a physically plausible solution particularly for the grassland sites where there were no additional complicating effects such as terrain and local discontinuities in vegetation cover (Kustas et al., 1994).

A sensitivity analysis of the set of equations used to compute the roughness parameters was conducted. The results suggest a sensitive inverse relationship between the magnitude of  $C_1$  and value of  $d_0$ , while all other constants (i.e.,  $C_2$  through  $C_4$ ) have a relatively minor impact on the estimation of  $d_0$ . If  $C_1$  was increased by 5% (0.95–1.0) the effect on predicted  $d_0$  was a reduction by nearly 40% while changes in  $z_0$  were relatively minor (Table 3). By changing  $C_1$ ,  $d_0$  results in general were more realistic, but not for the grass sites where  $d_0$  values remained greater than the height of the grass. The value of  $C_1$  was further increased to  $C_1 = 1.1$ , which is approximately midway between its observed range and the value used by Kustas et al. (1994) for semi-arid rangelands. This again resulted in relatively minor changes to  $z_0$  at all sites but physically unrealistic values for  $d_0$  ( $d_0 < 0$ ) at four of the five sites.

Table 1  
Values for the constants used in the variance formulations

Constant	Value
$C_1$	0.95
$C_2$	0.04
$C_3$	1.25
$C_4$	3



Table 2

Estimates of  $d_0$  and  $z_0$  using variance technique with values of constants defined in Table 1

Site	$h$ (m)	$d_0$ (m)	$z_0$ (m)
Grass-1	0.1	0.8	0.015
Grass-2	0.1	0.5	0.013
Transition	0.45	0.25	0.028
Shrub	0.5	0.55	0.027
Mesquite	1.5	0.9	0.043

Mean canopy/obstacle heights,  $h$ , for each site are listed.

Table 3

Estimates of  $d_0$  and  $z_0$  using variance technique with  $C_1 = 1$  and values of other constants defined in Table 1

Site	$h$ (m)	$d_0$ (m)	$z_0$ (m)
Grass-1	0.1	0.6	0.012
Grass-2	0.1	0.3	0.011
Transition	0.45	0	0.026
Shrub	0.5	0.3	0.025
Mesquite	1.5	0.5	0.038

Mean canopy/obstacle heights,  $h$ , for each site are listed.

As mentioned earlier, other studies using the variance approach for predicting scalar fluxes indicate that  $C_1$  may vary with surface type or land use (e.g., [Padro, 1993](#)). [Lloyd et al. \(1991\)](#) reported that the variation in  $C_1$  is significantly affected by the magnitude of  $d_0$  used in Eq. (3) or (5), particularly if the measurement height  $z$  is near the vegetation canopy. Another approach for computing  $d_0$  described in [De Bruin and Verhoef \(1997\)](#) was also attempted, but in many cases the resulting  $d_0 < 0$ , another physically unrealistic solution. This occurred even when selecting data to meet criteria that would most likely satisfy the free convective limit, namely when  $H_M > 150 \text{ W m}^{-2}$  and  $u < 2 \text{ m s}^{-1}$ . The results of the present study also suggest that the variance approach cannot be used to recover reasonable values for  $d_0$ .

Since physically realistic  $d_0$  values could not be obtained by the above set of equations, an alternative simple analytic expression from [Raupach \(1994, 1995\)](#) was employed to independently estimate  $d_0$  from the vegetation height ( $h$ ) and  $LAI$ . The form of this expression is

$$\frac{d_0}{h} = -1 \left[ \frac{1 - e^{(-\sqrt{cd_1}\Lambda)}}{\sqrt{cd_1}\Lambda} \right], \quad (6)$$

where  $cd_1$  is an empirical constant estimated from laboratory and field data to be on the order of 7.5 ([Raupach, 1994](#)) and  $\Lambda$  is the area index of the roughness elements that can be estimated from a leaf area index or a canopy area index. For this study we used the measured  $LAI$  as a surrogate for  $\Lambda$ . Using Eq. (6) resulted in more



constrained probable expressions of  $d_0 \sim 0.5h$ ,  $d_0 \sim 0.7h$  for the grass and mesquite sites respectively. Once the value of  $d_0$  was defined the value of  $C_1$  and  $z_0$  were computed again by iteration until both ratio's  $H_V/H_M$  and  $u_{*V}/u_{*U}$  approached unity. The resulting values of  $C_1$  and  $z_0$  are presented in Table 4. The values of  $C_1$  all fall within the range observed in previous studies, but the magnitudes did not correlate with cover type. Both the shrub and grass-2 sites have similar  $C_1$  values  $\approx 1$  while the transition and mesquite sites have  $C_1 \approx 0.95$  and the grass-1 site has  $C_1 \approx 1.1$ . There is little change in the original estimates of  $z_0$  using  $C_1 = 0.95$  for all sites (Table 2). This suggests that this approach can provide reasonable and robust estimates of  $z_0$  when  $d_0$  is determined independently.

Roughness parameters at the mesquite site were also estimated using the traditional wind profile technique. Wind profile data were selected for near-neutral conditions yielding nearly 300 observations. Aerodynamic roughness parameters computed from the wind profile technique and results reported by De Vries et al. (2001) who employed a remote sensing procedure using laser altimeter data (Menenti and Ritchie, 1994) for the same mesquite site were compared with results from the flux variance approach. Tables 5 and 6 present a comparison of the roughness parameters for three methods at the mesquite dune site. In Table 5 independent estimates of  $d_0$  from the wind profile, laser altimeter and Raupach's expression compared well with the wind profile method resulting in the largest  $d_0$  and the laser altimeter results the lowest. The combined average ratio of  $d_0/h$  for the three methods was 0.58. Table 6 show the results for  $z_0$  from the wind profile, laser altimeter and flux–variance approaches. The wind profile resulted in the largest estimate for  $z_0$  while the laser altimeter and flux–variance methods were identical. In general these

Table 4  
Estimate of  $z_0$  with a variable  $C_1$  and fixed  $d_0$  with values of the other constants defined in Table 1

Site	$h$ (m)	$C_1$ (-)	$d_0$ (m)	$z_0$ (m)
Grass-1	0.1	1.11	0.05	0.01
Grass-2	0.1	1.04	0.05	0.01
Transition	0.45	0.96	0.2	0.028
Shrub	0.5	1.02	0.2	0.024
Mesquite	1.5	0.94	1	0.044

Mean canopy/obstacle heights,  $h$ , for each site are listed.

Table 5  
Comparison of  $d_0$  for the mesquite site using wind profile, laser altimeter and Raupach 1994 (see text for details)

Technique	$d_0$ (m)
Wind profile	1
Laser altimeter	0.7
Raupach	0.9

Table 6  
Comparison of  $z_0$  for the mesquite site using wind profile, laser altimeter and variance technique (see text for details)

Technique	$z_0$ (m)
Wind profile	0.07
Laser altimeter	0.04–0.05
Variance	0.04–0.05

results indicate good agreement among the different approaches for estimating aerodynamic roughness parameters for a mesquite dune surface in an semi-arid environment.

4.2. Estimating sensible heat fluxes

The use of second order turbulent statistics with the flux–variance technique for estimating sensible heat fluxes has been investigated (e.g., Katul et al., 1996). This represents an alternative to Bowen-ratio and eddy covariance techniques for estimating latent and sensible heat fluxes in semi-arid regions. Important advantages of the flux–variance approach are simplicity of measurements (time series measurements of air temperature  $T_A$ , 2–10 Hz) and inexpensive instrumentation (compared with EC). In addition, flux–variance methods appear not to be affected by position within the roughness sub-layer and measurements are not constrained by flow distortion or wind direction as are more traditional aerodynamic methods (Kustas et al., 1994; Katul et al., 1995).

Using a global value for  $C_l$  ( $=1$ ), two estimates of  $H$  were computed. The first used the free convection assumption (Eq. (4)) and the second, the full expression which included the influence of mechanical transport (Eq. (3)). The  $u_*$  values were computed by iteration using the roughness parameters from Table 4 and wind speed observations with Eqs. (1) and (2). Note that neither approach use  $H_M$  when computing an estimate. Results are shown in Fig. 1(a) and (b). For the case that includes the effects of mechanical transport via Eqs. (1)–(3), estimates of  $H$  compared well with those from eddy covariance resulting in a root mean square error (RMSE) of  $30 \text{ W m}^{-2}$  and an  $r^2 = 0.85$ . For the free convective case, (Eq. (4)) Fig. 1(b) shows more scatter, higher RMSE  $40 \text{ W m}^{-2}$ , and an  $r^2 = 0.74$ . More variability was observed using Eq. (4) relative to Eq. (3). This suggests that effects of momentum transport need to be accounted for even under conditions approaching the free convective limit and should be included in sensible heat flux computations when possible.

5. Summary and conclusions

A method that combines sensible heat flux measurements from eddy co-variance with flux–variance relationships was investigated to compute aerodynamic

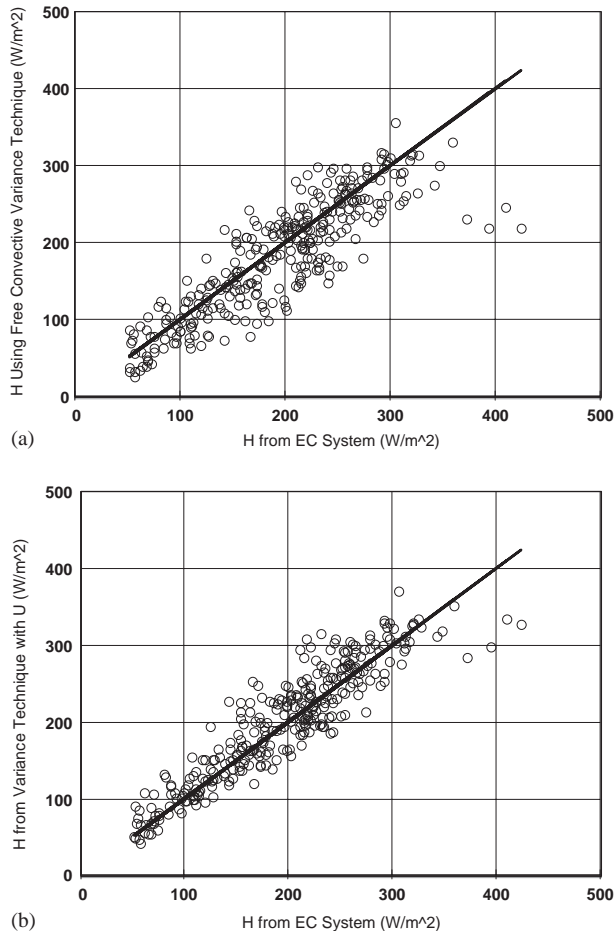


Fig. 1. (a)  $H$  estimated using flux–variance technique for temperature under the free convective limit (i.e., Eq. (4)) versus eddy covariance measurements. Line is 1:1, (b)  $H$  estimated using flux–variance technique for temperature versus eddy covariance measurements with the influence of mechanical turbulence included (i.e., Eq. (3)) where  $u_*$  is estimated from Monin Obukhov similarity, Eqs. (1) and (2) (see text). Line is 1:1.

roughness parameters for a semi-arid rangeland. This is an operational technique for estimating  $H$  requiring only high frequency measurements of air temperature, wind speed observations, and reliable estimates of  $z_0$  and  $d_0$ . The method computed reasonable values of roughness length ( $z_0$ ) for all sites that were of a comparable magnitude with reported values of other semi-arid landscapes. Roughness length estimates at the mesquite dune site compared well with those computed independently from wind profile and remotely sensed laser altimeter data. Displacement height,  $d_0$ , results were mixed and were strongly dependent on the value of the constant  $C_1$ . For grass surfaces, unrealistic values of  $d_0$  resulted.

However, the estimated mesquite  $d_0$  values appear to be physically reasonable. An alternative approach was examined that also did not provide reliable  $d_0$  estimates for this plant community. The estimates of  $z_0$  were not strongly affected by the values of  $d_0$ .

The grass sites had  $z_0 \sim 0.01$  m, the shrub and transition sites with slight topography had  $z_0 \sim 0.025$  m, while the mesquite dune site resulted in  $z_0 \sim 0.045$  m. However, the magnitude of  $C_1$  was not strongly correlated to land cover type and thus cannot be estimated a priori. Estimates of sensible heat flux using the variance approach compared well (mean  $r^2 = 0.80$ ) with eddy covariance measurements. Improved agreement was obtained by including contributions of mechanical transport in the formulation. Since roughness parameters are critical to modeling the surface energy and water balance of semi-arid landscapes, it is important to develop theoretically sound and robust methods for estimating roughness parameters for semi-arid landscapes.

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